

Embry-Riddle Aeronautical University

Department of Physical Sciences

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Multiple Spacecraft Autonomous Systems:

Theoretical Research & Laboratory Experimentation

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NAVAL
POSTGRADUATE
SCHOOL

Spacecraft Robotics
LABORATORY

Outline

- ❑ Myself and the NPS team
- ❑ Goals of research on Multiple Spacecraft Autonomous Systems
- ❑ Motivation of the research topic



Theoretical Results: low propellant maneuvers by differential drag-based analytical controller (PURE RESEARCH)



Experimental Results: LQR CONTROL and INPUT ESTIMATION applied to a four spacecraft simulator assembly (APPLIED RESEARCH)



EMBRY-RIDDLE
AERONAUTICAL UNIVERSITY

Plans for research and teaching at Embry-Riddle

My story at a glance



M. Sc. In Aerospace Engineering from *Sapienza University, Rome, Italy, 2002.*



Project Engineer in Mission Analysis at *Grupo Mecanica del Vuelo, Madrid, Spain, 2003.*



Ph. D. in Applied Mathematics, Aerospace Engineering focus, from *Sapienza University, Rome, Italy, 2007.*



Post-Doctoral appointment at NPS (my beautiful wife followed me in this latest adventure!)

- Spacecraft Robotics Laboratory Manager*
- Teaching Assistant for Mechanics, Orbital Mechanics, Spacecraft Attitude Determination and Control*
- Laboratory developed Theses co-advisor*

Myself and the NPS

I am here

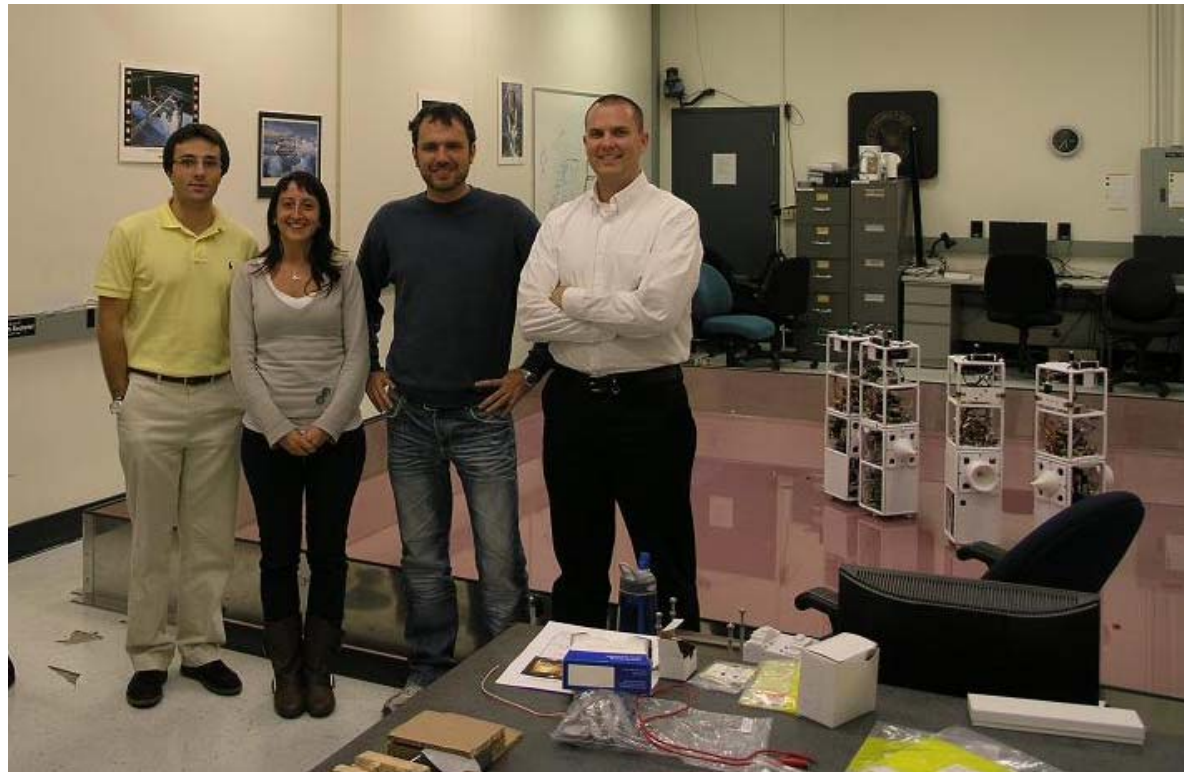


Working on the spacecraft simulators



The SRL team

Myself and international students/interns



- ❑ **Guidance, Navigation, and Control for robust autonomous multiple spacecraft rendezvous/assembly/reconfiguration**
 - Flexibility towards the evolving system
 - Scalability to an arbitrary number of spacecraft
 - Homogeneous and heterogeneous spacecraft

- ❑ **Optimize resources** to allow repeated maneuvering. Consider alternative control methods (differential drag)

- ❑ **Hardware-in-the-loop validation: sponsored research & great educational value**

Multiple S/C systems allow for low-cost orbit insertion, reconfiguration-ability, upgrade-ability...

NASA'S MISSIONS TO MOON AND MARS WILL BE BASED ON TWO ON-ORBIT DOCKING CAPSULES

CURRENT AND PAST

- ❑ Differential drag missions:
 - **JC2Sat**: joint Canadian-Japanese
 - **InKlajn-1**: Israeli Nano-Satellite Association
- ❑ **ESA Automated Transfer Vehicle (ATV, ISS re-supply vehicle)**
- ❑ **DARPA Orbital Express, 2007**
- ❑ **NASA DART, 2005**
- ❑ National Space Development Agency of Japan's **ETS-VII** in 1998

FUTURE

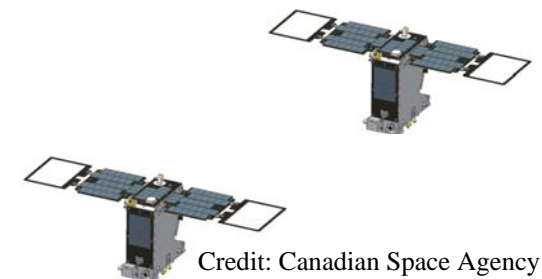
- ❑ **AFRL's Autonomous Nano-satellite Guardian Evaluating Local Space (ANGELS)**
- ❑ **DARPA F6 System**



Credit: Defense Advanced Research Projects Agency



Credit: European space Agency



Credit: Canadian Space Agency

Theoretical Results: Differential Drag

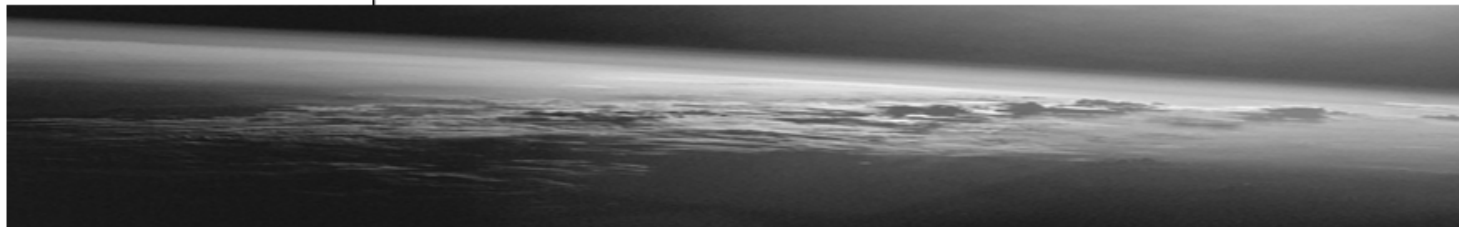
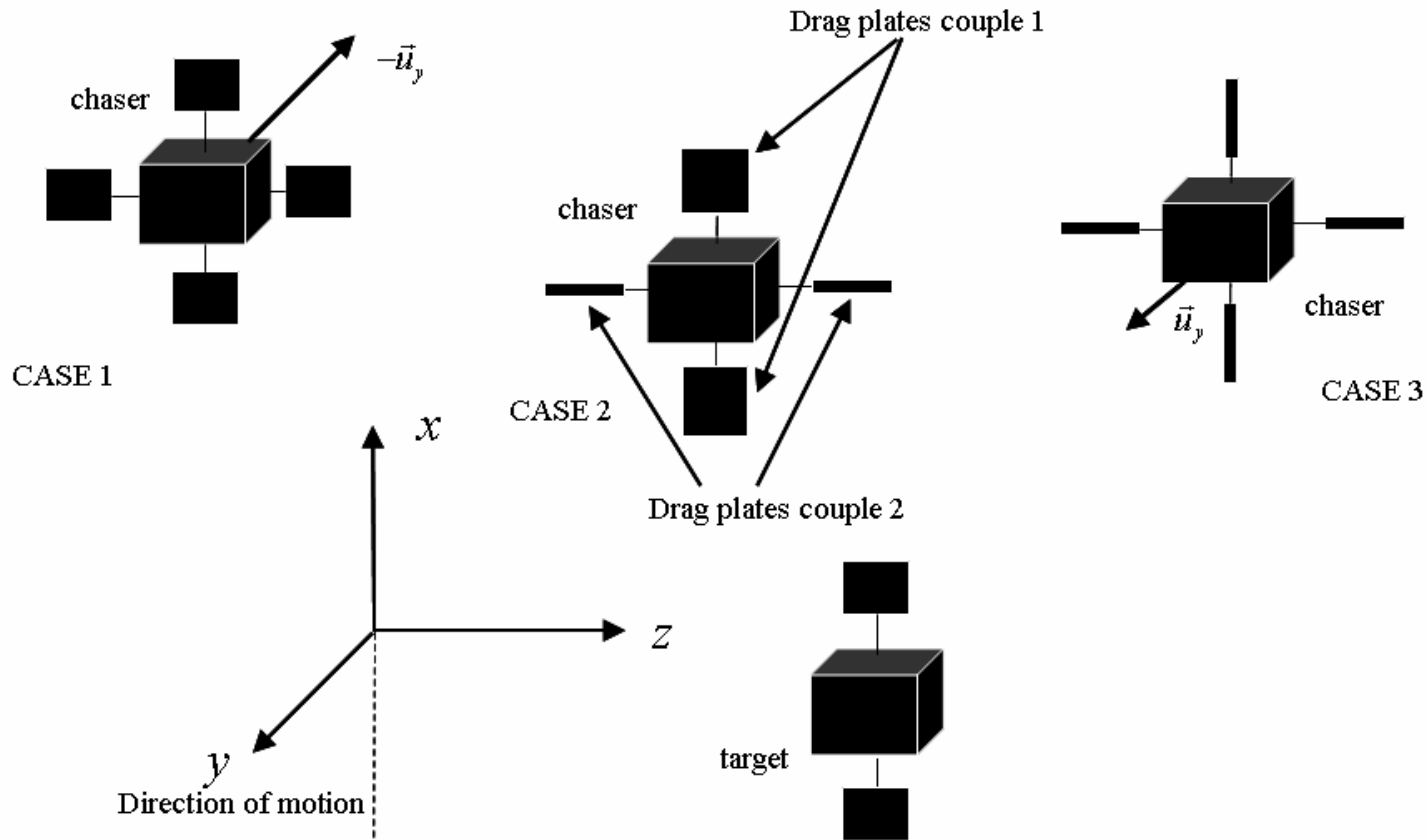
- ❑ Starting references and related work
- ❑ Use differential drag to assemble small spacecraft from a distance of ~3-5 Km
- ❑ Include J2 differential effects due to long time duration maneuvers
- ❑ **Develop an analytical control policy capable of assembling N heterogeneous satellites controlled by differential atmospheric drag**
- ❑ Concept proposed for spacecraft with virtually on-off surface control capability
- ❑ Demonstrate the control policy capabilities in a complete simulation environment (orbital propagator, non-constant density, navigation errors, etc. ...)

Starting References & Related Work

- 1) Leonard, C. L., Hollister, W. M., and Bergmann, E. V., “Orbital Formationkeeping with Differential Drag,” *Journal of Guidance, Control, and Dynamics*, Vol. 12, No. 1, 1989, pp. 108–113. doi:10.2514/3.20374
- 2) Schweighart, S. A., and Sedwick, R. J., “High-Fidelity Linearized J2 Model for Satellite Formation Flight,” *Journal of Guidance, Control, and Dynamics*, Vol. 25, No. 6, 2002, pp. 1073–1080.
- 3) Maclay, T., Tuttle, C., 2005, “Satellite Stationkeeping of the ORBCOMM Constellation Via Active Control of Atmospheric Drag: Operations, Constraints, and Performance”, *Advances in Astronautical Sciences*, Vol. 120, Part I, pp. 763-773.
- 4) Palmerini, G. B., Sgubini, S., and Taini, G., “Spacecraft Orbit Control Using Air Drag,” *International Astronautical Congress Paper 05-C1.6.10*, 2005.
- 5) Campbell, M. E., “Planning Algorithm for Multiple Satellite Clusters,” *Journal of Guidance, Control, and Dynamics*, Vol. 26, No. 5, 2003, pp. 770–780.
- 6) Guelman, M., and Aleshin, M., “Optimal Bounded Low-Thrust Rendezvous with Fixed Terminal-Approach Direction,” *Journal of Guidance, Control, and Dynamics*, Vol. 24, No. 2, 2001, pp. 378–385.

Concept for generating differential drag

Attitude is stabilized in the orbital frame LVLH



Dynamics & working assumptions for analytical derivations

$$\dot{\mathbf{x}} = \begin{bmatrix} \mathbf{0}_{2 \times 2} & \mathbf{I}_{2 \times 2} \\ \mathbf{A}_1 & \mathbf{A}_2 \end{bmatrix} \mathbf{x} + \begin{bmatrix} \mathbf{0}_{2 \times 2} \\ \mathbf{I}_{2 \times 2} \end{bmatrix} \mathbf{u} \quad \mathbf{x}(t) \in \mathbb{R}^4, \forall \mathbf{x}^T = [x, y, \dot{x}, \dot{y}]$$

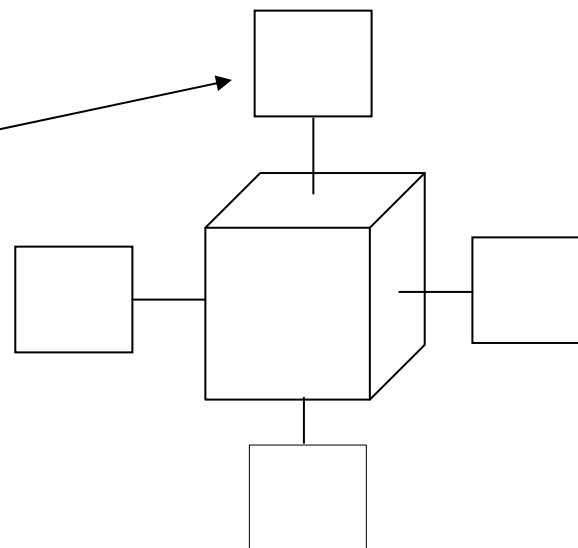
$$\mathbf{A}_1 = \begin{bmatrix} 5c^2\omega^2 - 2\omega^2 & 0 \\ 0 & 0 \end{bmatrix}, \mathbf{A}_2 = \begin{bmatrix} 0 & 2\omega c \\ -2\omega c & 0 \end{bmatrix} \longrightarrow \text{Schweighart-Sedwick Dynamics}$$

$$\mathbf{u}^T = \left[0 \quad -\frac{\rho \Delta BC}{2} V_r^2 \right] \longrightarrow \text{Because relative velocity is negligible with respect to the orbital one}$$

$$\Delta BC = BC_{C_i} - BC_T = \frac{m_T C_{D_{C_i}} S_{C_i} - m_{C_i} C_{D_T} S_T}{m_T m_{C_i}} \longrightarrow \text{Heterogeneous spacecraft (similar parameters)}$$

◆ On-off control (0-90 deg)

◆ Constant air density



Dynamics Model: the state vector transformation

Linear state vector
transformation

$$\mathbf{z} = \begin{bmatrix} 0 & 1 & -a/d^2 & 0 \\ -ab/d^2 & 0 & 0 & -b/d^2 \\ 0 & 0 & a^2/(2d^3) & 0 \\ a^2b/(2d^3) & 0 & 0 & a^3/(2d^3) \end{bmatrix} \mathbf{x}$$

State analytical
evolution

$$z_1 = z_{1_0} + tz_{2_0} - \frac{bt^2}{2d^2} u_y$$

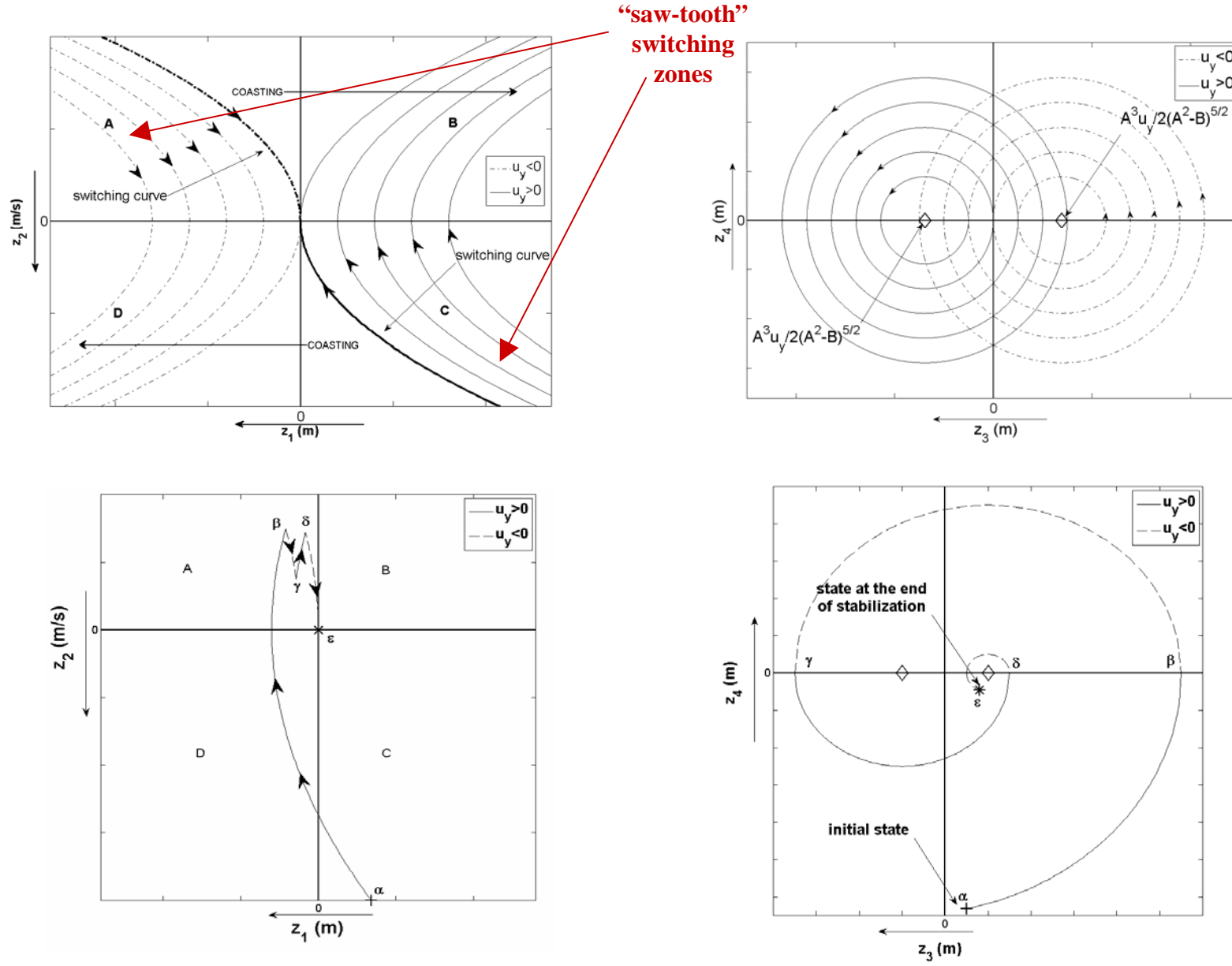
$$z_2 = z_{2_0} - \frac{bt}{d^2} u_y$$

$$z_3 = \cos(dt) z_{3_0} + \frac{\sin(dt)}{d} z_{4_0} + \frac{a^3 [1 - \cos(dt)]}{2d^5} u_y$$

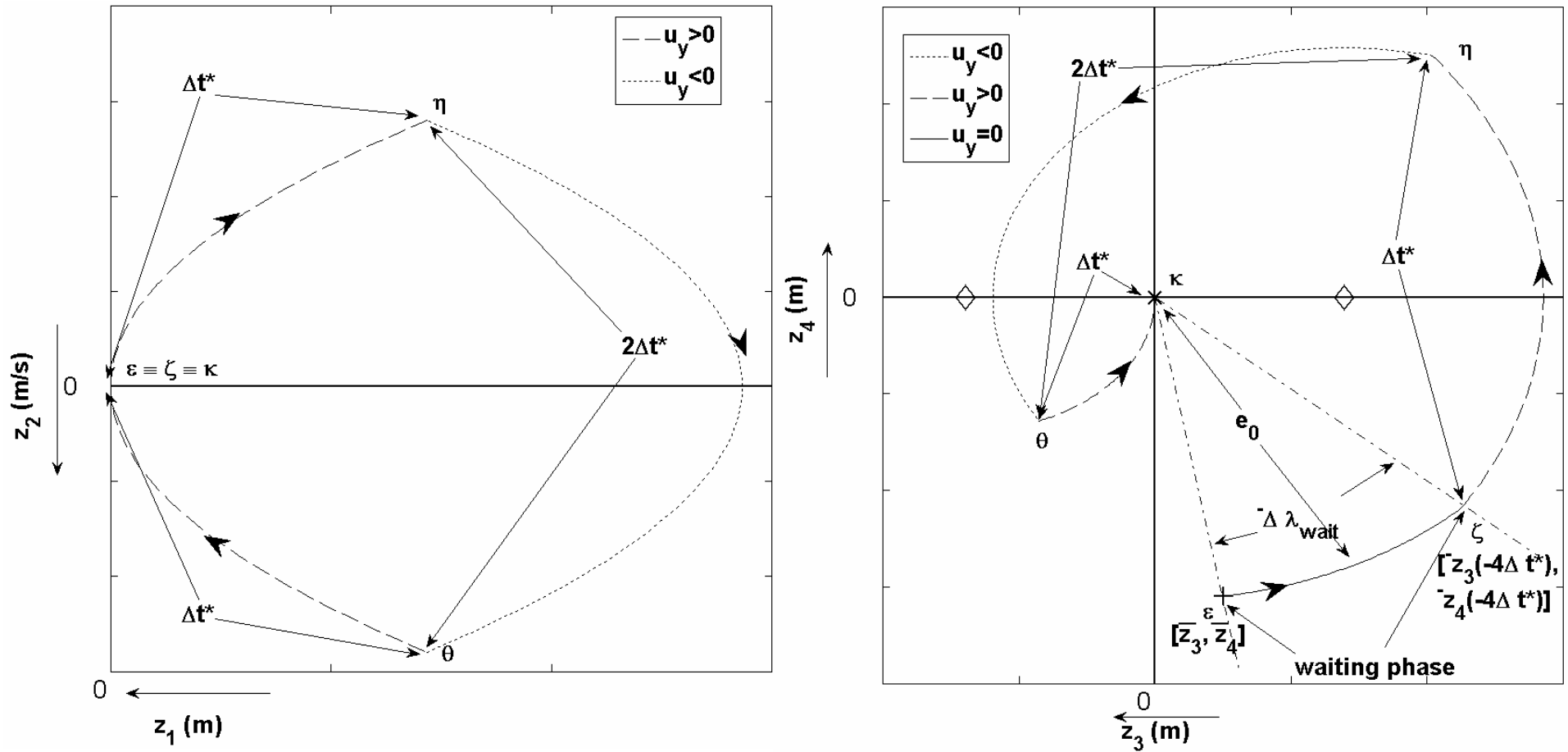
$$z_4 = -d \sin(dt) z_{3_0} + \cos(dt) z_{4_0} + \frac{a^3 \sin(dt)}{2d^4} u_y$$

$$a = 2\omega c, b = (5c^2 - 2)\omega^2, d = \sqrt{a^2 - b}$$

Stabilization: (based on Leonard's work)



Analytical Exact Rendezvous to Target



NO RESIDUAL DISTANCE IS PRESENT.

Exact Rendezvous to Target: the solution

$$\Delta t^* = \frac{1}{d} \cos^{-1} \left[\frac{1}{2} \left(1 + \sqrt{h} - \sqrt{3 - h - \frac{2}{\sqrt{h}}} \right) \right] \longrightarrow \text{Generic formula for the maneuvering time}$$

$$h = 1 + \frac{\sqrt[3]{f}}{6g} - \frac{e_0^2}{g\sqrt[3]{f}}$$

$$f = -54ge_0^2 + 6\sqrt{3}e_0^2\sqrt{2e_0^2 + 27g^2}$$

$$g = -\frac{\sqrt{2}}{2} \frac{a^3 |u_y|}{d^5} i$$

$$e_0 = \sqrt{z_3^2 + (z_4/d)^2} < \frac{13}{5} \frac{a^3 |u_y|}{d^5} \longrightarrow \text{CONSTRAINT: Condition to go at zero with only one sequence...}$$

$$e_0 = e_0 - .99 \left(\frac{13}{5} \frac{a^3 |u_y|}{d^5} \right) \longrightarrow \text{...otherwise the sequence is applied to reach an harmonic motion of smaller amplitude}$$

TIME TO ZERO OUT THE FULL STATE IS PREDICTABLE

Orbital Parameters and Spacecraft Characteristics

Table 1. Simulations Parameters

m_T (kg)	10
m_{C_1} (kg)	11
m_{C_2} (kg)	9
S_P (m ²)	.25
S_T (m ²)	.75
$S_{C_1, \min}, S_{C_1, \min}$ (m ²)	.25
$S_{C_1, \max}, S_{C_1, \max}$ (m ²)	1.25
$S_{C_1, 0}$ (m ²)	.7857
$S_{C_2, 0}$ (m ²)	.7105
C_{D_1}	2.2
C_{D_2}	2.31
C_{D_3}	2.09
$\Delta BC_{C_1, \max}$ (m ² /kg)	.0975
$\Delta BC_{C_1, \min}$ (m ² /kg)	.1253
$\Delta BC_{C_2, \min}$ (m ² /kg)	-.1125
$\Delta BC_{C_3, \min}$ (m ² /kg)	-.107
$h(t_0)$ (km)	356
F_{\max} (mN)	5
Δt_{opt} (s)	100

Table 2. Target Spacecraft Initial Conditions

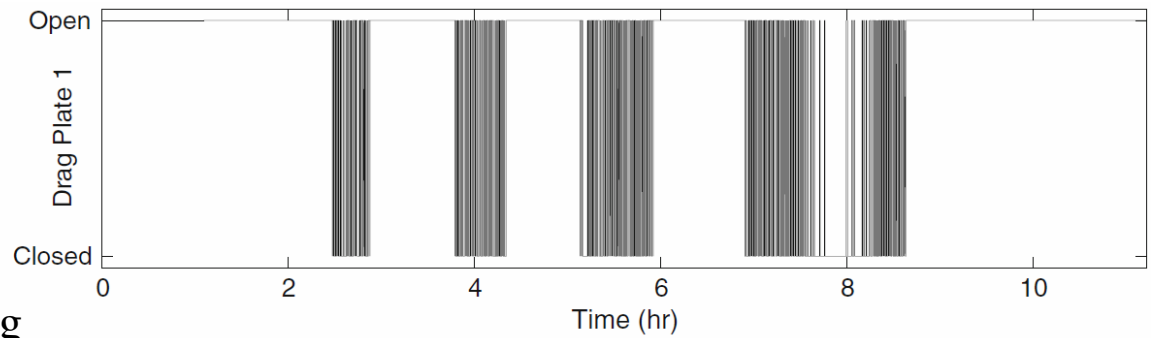
$a_T = 6713889.83$ m
$e_T = 0.01$
$i_T = 51.9412$ deg
$\Omega_T = 206.3577$ deg
$\omega_T = 101.0711$ deg
$\nu_T = 108.0848$ deg

Table 3. Chaser Spacecraft Initial Positions in LVLH

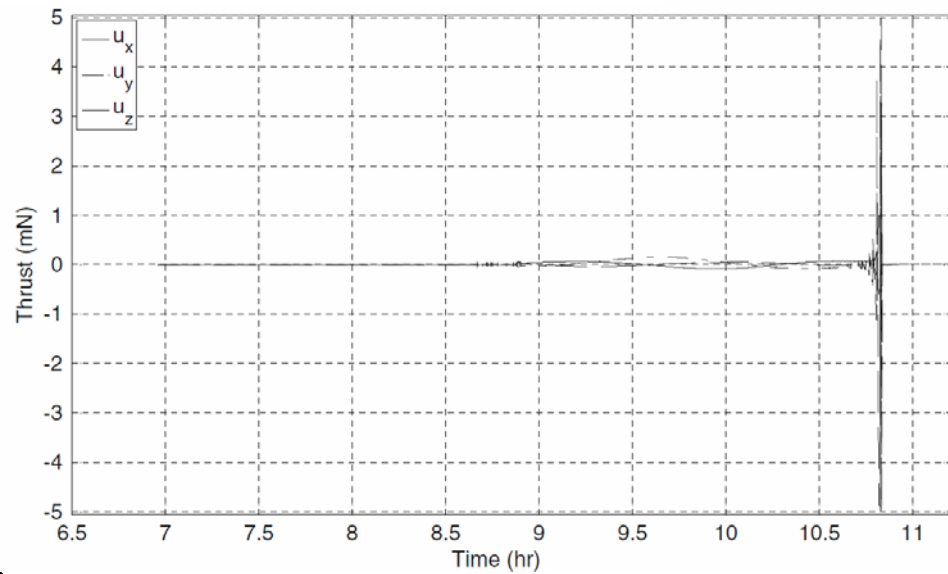
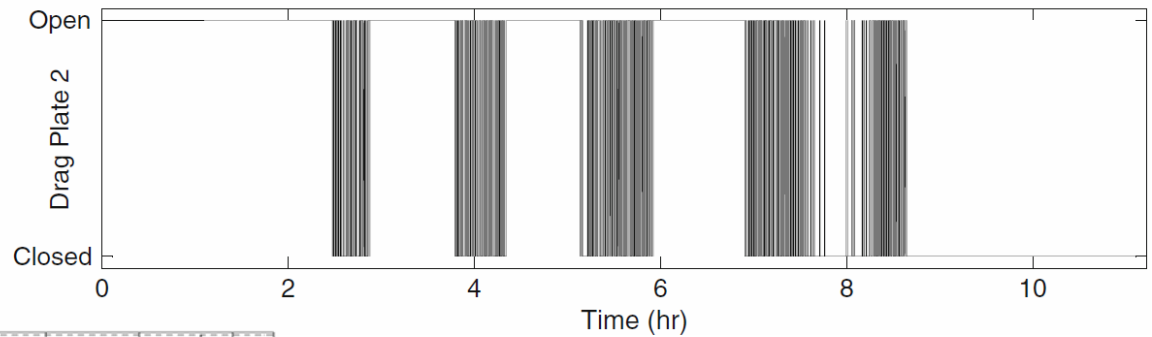
$\mathbf{r}_{C_1}(t_0)$ (m)	[1000, 2000, 10]
$\mathbf{r}_{C_2}(t_0)$ (m)	[-1000, -2000, -10]
$\mathbf{v}_{C_2}(t_0)$ (m/s)	[-.0084, -1.7018, -.0063]
$\mathbf{v}_{C_3}(t_0)$ (m/s)	[.0094, 1.7020, .0063]

- Non constant density, 30% uncertainty
- Plates have dynamics (10 seconds)
- Full orbital model
- Navigation errors

Simulation: 2 chasers, drag & optimal thrust

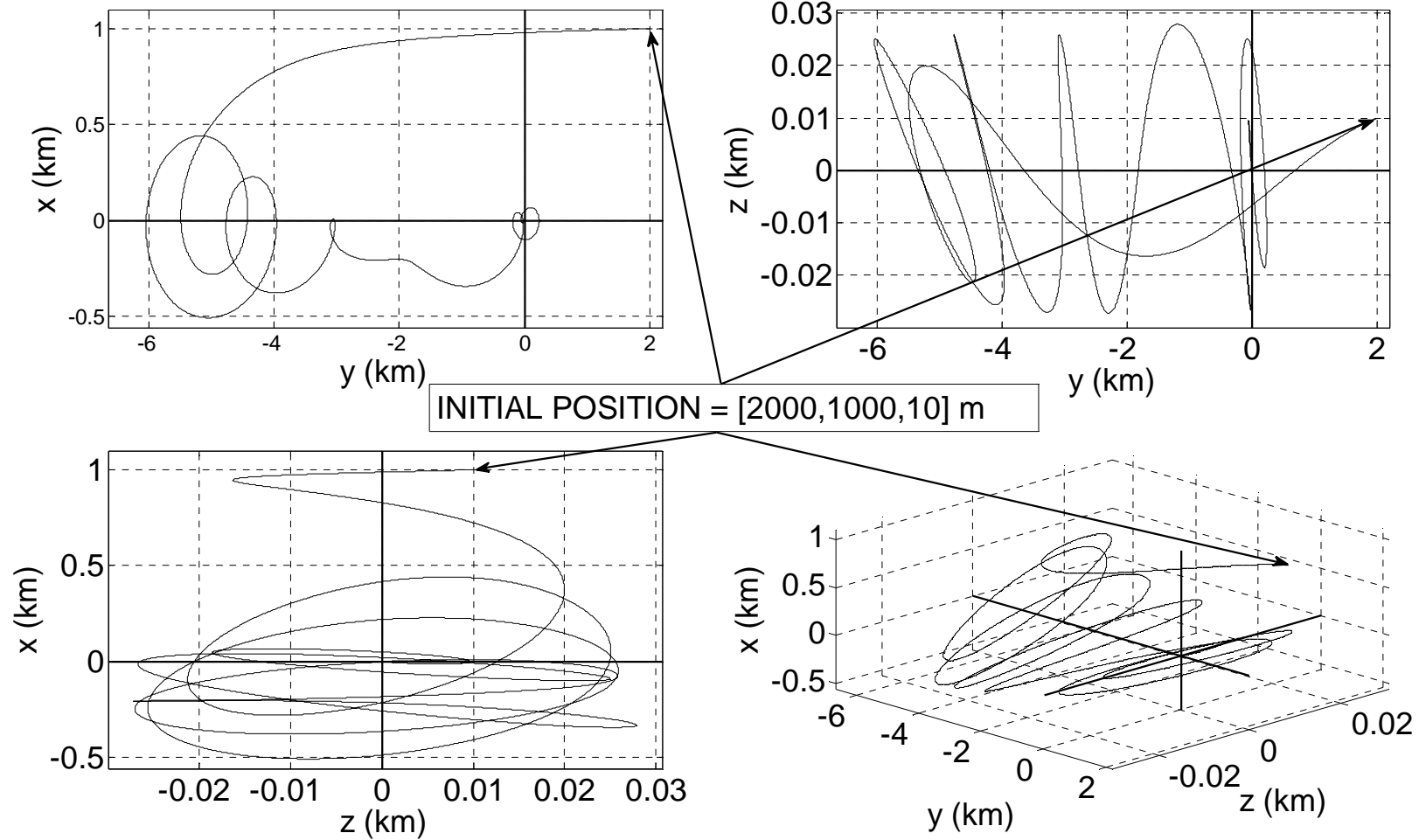


Phase 1: only differential drag

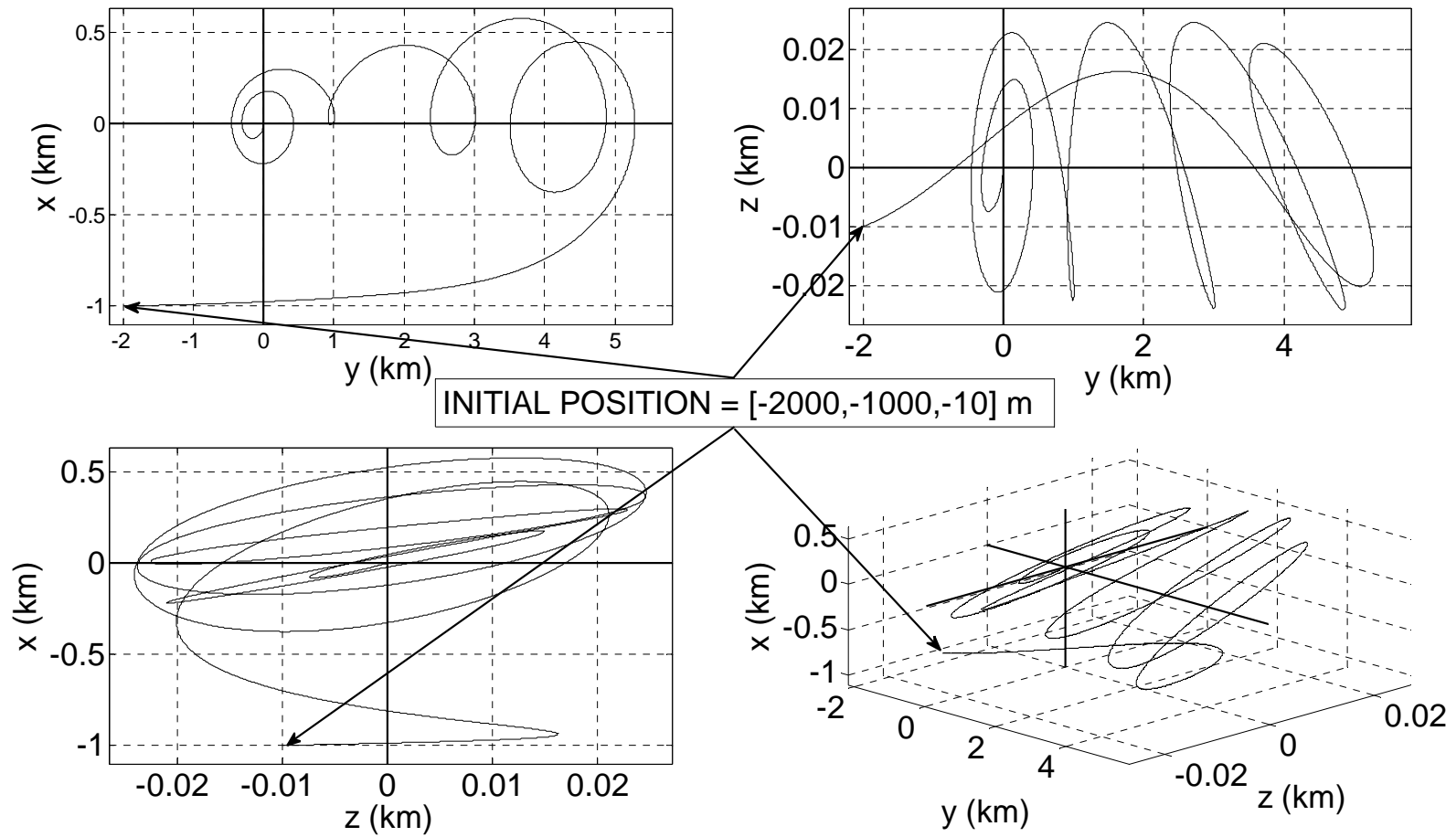


Phase 2: only thrusters

Simulation: 2 chasers, drag & optimal thrust



Simulation: 2 chasers, drag & optimal thrust



Simulation results

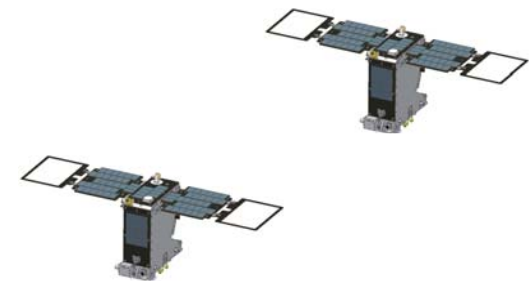
Table 4. Simulation Test Case 1 Results: Fuel Consumption and Starting points for the Low-Thrust phase

Chaser 1	Chaser 2
$I = 2.18 \text{ mNs}$	$I = 19.4 \text{ mNs}$
$\Delta V = 2 \times 10^{-4} \text{ m/s}$	$\Delta V = 2 \times 10^{-3} \text{ m/s}$
Thrusting Start: $\mathbf{r}_{c_1} (m) = [-58.75, -148.45, 21.54]$	Thrusting Start: $\mathbf{r}_{c_2} (m) = [-47.83, -440.90, -7.75]$
Total Maneuver Time: 10.83 hours	Total Maneuver Time: 9.33 hours

Table 5. Simulation Test Case 2 Results: Fuel Consumption

Chaser 1	Chaser 2
$I = 40.5 \text{ mNs}$	$I = 19.8 \text{ mNs}$
$\Delta V = 3.68 \times 10^{-3} \text{ m/s}$	$\Delta V = 2.21 \times 10^{-2} \text{ m/s}$
Total Maneuver Time: 10.14 hours	Total Maneuver Time: 8.68 hours

Saving more than 90% Delta V



- 1) **Bevilacqua, R.**, Hall, J., S., Romano, M., “Multiple Spacecraft Assembly Maneuvers by Differential Drag and Low Thrust Engines”, *Celestial Mechanics and Dynamical Astronomy*, Volume 106, Issue 1 (2010), p. 69-88.

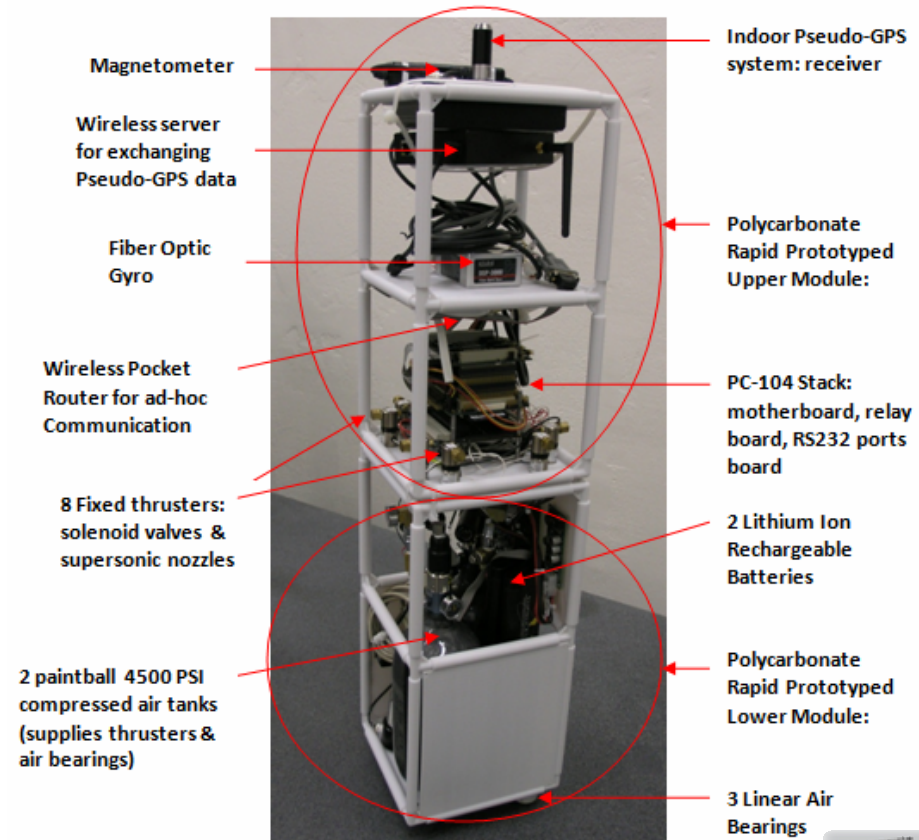
- 2) **Bevilacqua, R.**, Romano, M., Curti, F., “Decoupled-natural-dynamics model for the Relative Motion of two Spacecraft without and with J2 perturbation”, accepted for publication, to appear on the *Nonlinear Dynamics and Systems Theory* (2009).

- 3) **Bevilacqua, R.**, Romano, M., “Non-propellant Rendezvous Maneuvers of Multiple Spacecraft by Differential Drag under J2 Perturbation”, *AIAA Journal of Guidance, Control and Dynamics*, vol.31 no.6 (1595-1607), 2008.

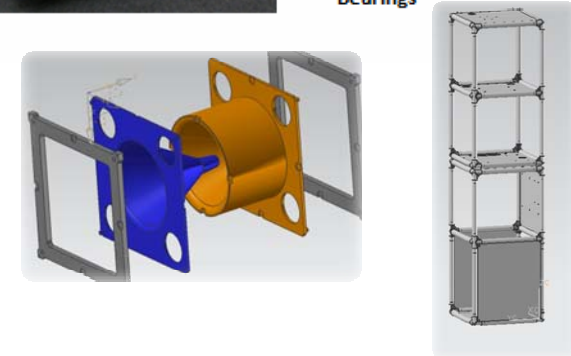
Experimental Results: Outline

- ❑ Starting references and related work
- ❑ Sub-Optimal Attitude-Position Control via Linear Quadratic Regulator
- ❑ Spacecraft Simulators at the Spacecraft Robotics Laboratory
- ❑ Specializing the LQR Problem to the 3 DOF Spacecraft Simulators
- ❑ Control during Docking: plume impingement
- ❑ Briefly on Input Estimation
- ❑ Experimental Results

Spacecraft Simulators at the Spacecraft Robotics Lab



- ▶ **Ad-hoc wireless communication**
- ▶ **Modularity**
- ▶ **Small footprint (20x20 cm)**
- ▶ **Light weight (10 kg)**
- ▶ **Rapid Prototyping: fast integration of new structural parts, custom designed**



Starting References & Related Work

- 1) Frost, S. A., Balas, M. J., “Adaptive Key Component Controllers for Evolving Systems,” AIAA Guidance, Navigation and Control Conference and Exhibit, 18 - 21 August 2008, Honolulu, Hawaii, AIAA 2008-6279.
- 2) Dong, S., Allen, K., et al., “Self-assembling wireless autonomously reconfigurable module design concept,” ACTA Astronautica, vol. 62, pages 246-256, Jan 2008.
- 3) Romano, M., Friedman, D.A., Shay, T.J. , “Laboratory Experimentation of Autonomous Spacecraft Approach and Docking to a Collaborative Target,” AIAA Journal of Spacecraft and Rockets, Vol. 44, No. 1, pp. 164-173, January-February 2007.
- 4) Toglia, C., Kettler, D., Kennedy, F., Dubowsky, S., “A Study of Cooperative Control of Self-Assembling Robots in Space with Experimental Validation,” 2009 IEEE International Conference on Robotics and Automation, May 12 - 17, 2009, Kobe, Japan.

Different phases of the LQR-driven control

□ RENDEZVOUS $|\vec{r}_{rsw}| > r_{dock}$

□ DOCKING APPROACH $|\vec{r}_{rsw}| \leq r_{dock}$

a. within the docking cone

- $|\vec{r}_{rsw}| > r_{imp}$ keep maneuvering
- $|\vec{r}_{rsw}| \leq r_{imp}$ impingement: thrusters off

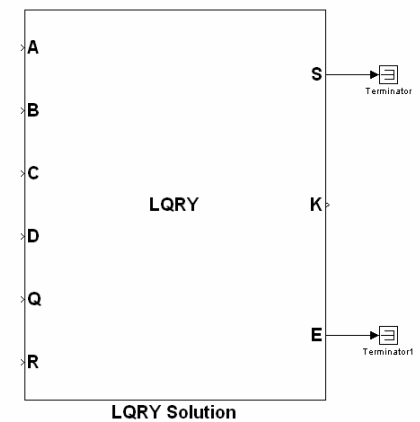
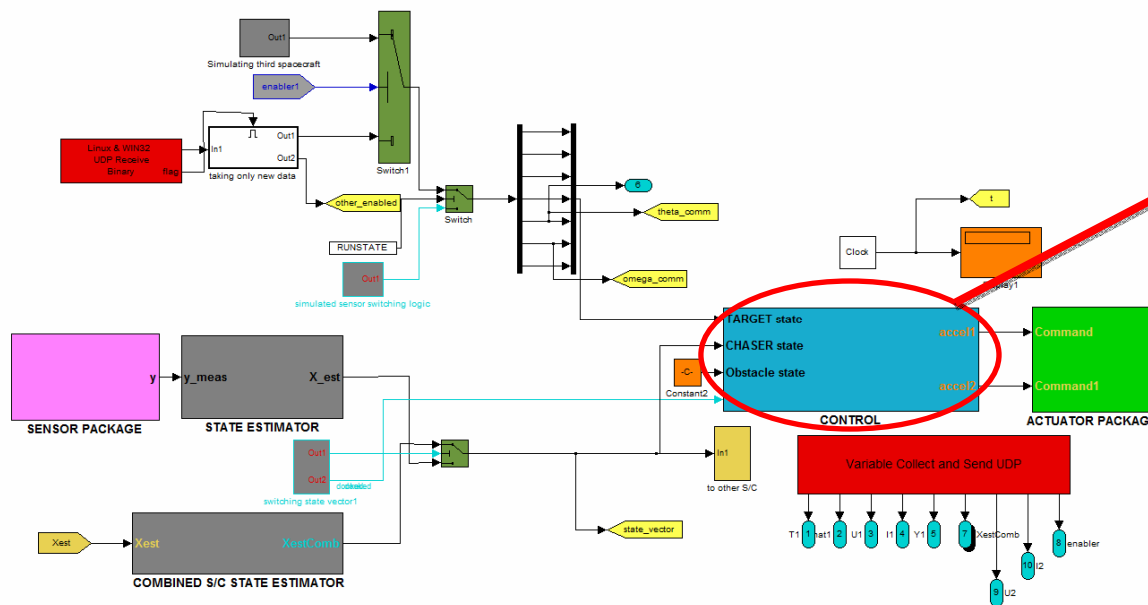
b. outside docking cone \longrightarrow orbiting to gain time while attitude is corrected

Real Time onboard OS and Rapid Prototyping of Executables

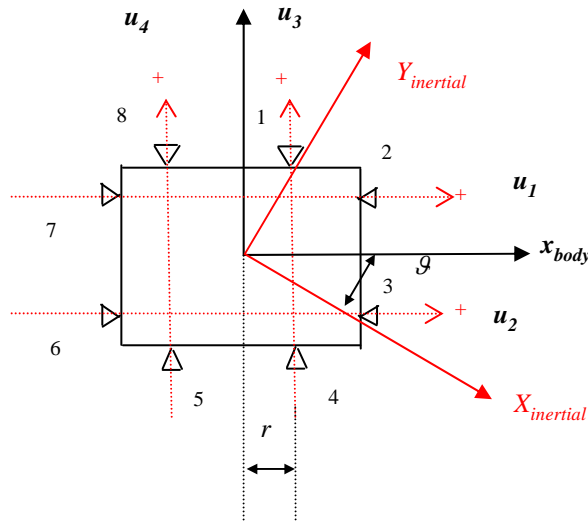
Programming and simulations on Simulink

Automatic generation of C code for RTAI Linux (simulators onboard OS)

Compilation of the C code into a real time executable



Specializing the LQR Problem to the 3 DOF Simulators: one spacecraft



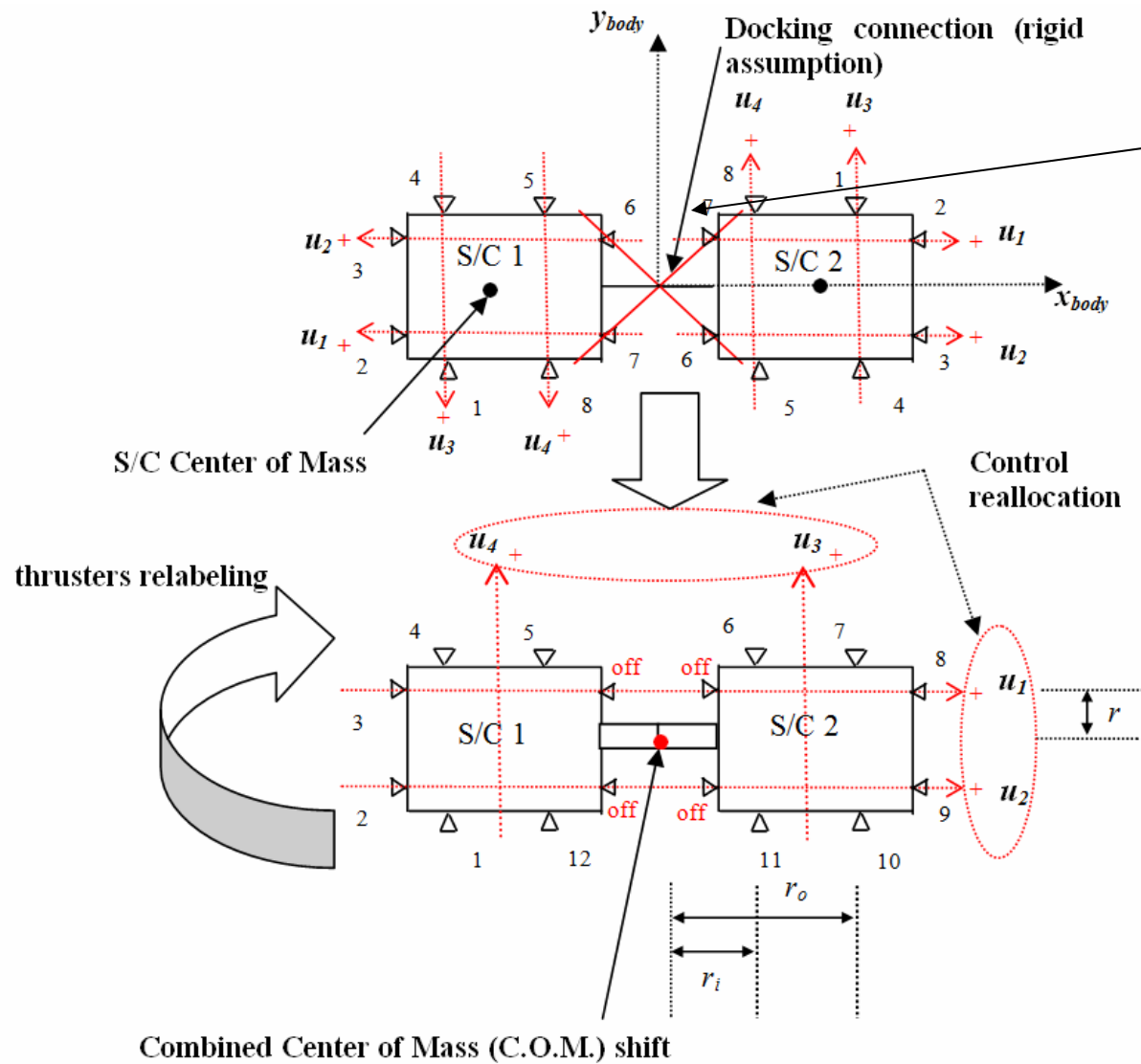
$$\vec{u} = [u_1, u_2, u_3, u_4]^T$$

$$A = \begin{pmatrix} 0_{3 \times 3} & I_{3 \times 3} \\ 0_{3 \times 3} & 0_{3 \times 3} \end{pmatrix}, B = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ \frac{\cos(\vartheta)}{m} & \frac{\cos(\vartheta)}{m} & \frac{-\sin(\vartheta)}{m} & \frac{-\sin(\vartheta)}{m} \\ \frac{\sin(\vartheta)}{m} & \frac{\sin(\vartheta)}{m} & \frac{\cos(\vartheta)}{m} & \frac{\cos(\vartheta)}{m} \\ \frac{-r}{J_z} & \frac{r}{J_z} & \frac{r}{J_z} & \frac{-r}{J_z} \end{pmatrix}, C = I_{6 \times 6}, D = 0_{6 \times 4}$$

Linearizing attitude about current commanded orientation

$$B_{LIN} = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ \frac{\cos(\vartheta_{des}) - \sin(\vartheta_{des})(\vartheta - \vartheta_{des})}{m} & \frac{\cos(\vartheta_{des}) - \sin(\vartheta_{des})(\vartheta - \vartheta_{des})}{m} & \frac{-\sin(\vartheta_{des}) + (\cos(\vartheta_{des}))(\vartheta - \vartheta_{des})}{m} & \frac{-\sin(\vartheta_{des}) + (\cos(\vartheta_{des}))(\vartheta - \vartheta_{des})}{m} \\ \frac{\sin(\vartheta_{des}) + (\cos(\vartheta_{des}))(\vartheta - \vartheta_{des})}{m} & \frac{\sin(\vartheta_{des}) + (\cos(\vartheta_{des}))(\vartheta - \vartheta_{des})}{m} & \frac{\cos(\vartheta_{des}) - \sin(\vartheta_{des})(\vartheta - \vartheta_{des})}{m} & \frac{\cos(\vartheta_{des}) - \sin(\vartheta_{des})(\vartheta - \vartheta_{des})}{m} \\ \frac{-r}{J_z} & \frac{r}{J_z} & \frac{r}{J_z} & \frac{-r}{J_z} \end{pmatrix}$$

Specializing the LQR Problem to the 3 DOF Simulators: two spacecraft



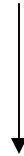
Control during docking
6 & 7 are shut off

Mass and mass distribution along with number and location of engines are the only new values

Input Estimation for S/C Relative Navigation

What if sensors' updates are slow (e.g.: every 2 seconds) + random interruptions?

Each S/C needs to estimate where its target fellow is, between updates



...BUT IT DOES NOT KNOW THE OTHER S/C MANEUVERS...



Kalman Filter for Relative Position, Velocity, and ESTIMATING THE OTHER S/C CONTROLS (INPUTS): THEY BECOME PART OF THE ESTIMATED STATE

Experimental Results: full experiment with four spacecraft simulators

VIDEO

<http://www.vimeo.com/8357179>

- 1) **R. Bevilacqua**, J. Hall, J. Horning, M. Romano, Ad-hoc Wireless Networking and Shared Computation based upon Linux for Autonomous Multi-Robot Systems, *AIAA Journal of Aerospace Computing, Information, and Communication*. Vol. 6, No 5, pp. 328-353, May 2009. Doi: 10.2514/1.40734.

- 2) **Bevilacqua, R.**, Lehmann, T., Romano, M., “Development and Experimentation of a LQR/APF Control for Autonomous Proximity Maneuvers of Multiple Spacecraft,” submitted for publication to *Acta Astronautica*.

- 3) Curti, F., Romano, M., **Bevilacqua, R.**, “Model Based Thruster Commanding for Rotational and Translational Control of a Spacecraft”, submitted for possible publication on the *AIAA Journal of Guidance, Control and Dynamics*.

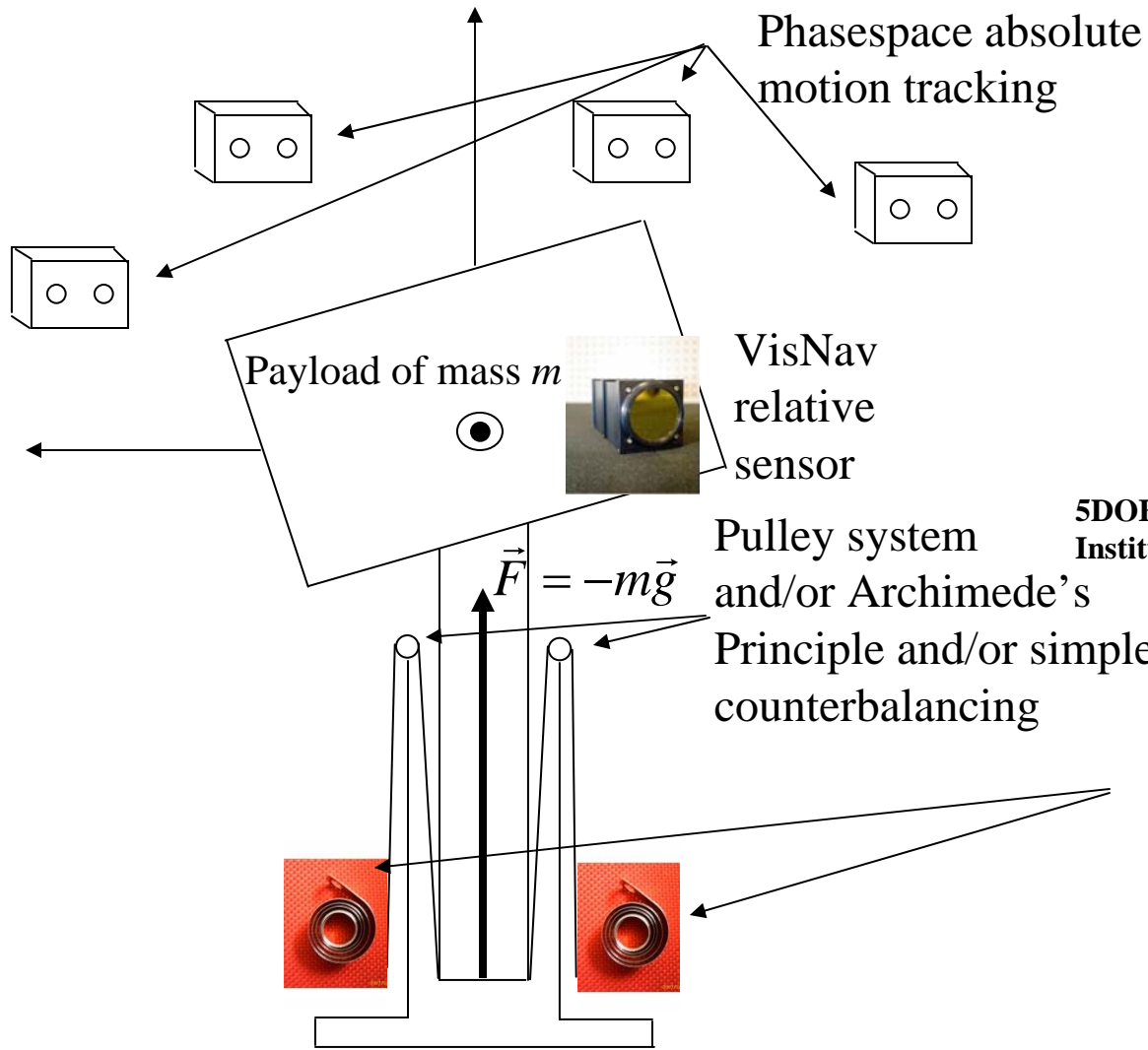
Plan for Research at Embry-Riddle

- ❑ **Differential Drag**: extend to eccentric LVLH & use JC2Sat feedback
- ❑ **Build a 6 degrees of freedom spacecraft simulators test-bed...potential extension: robotic manipulators installed**
- ❑ **Complete the guidance and relative tracking**
 - GUIDANCE (high level consensus reaching on sequence of assembly);
 - NAVIGATION (Input-Estimation spacecraft relative tracking).
- ❑ **Develop Sub-Optimal Real Time** technique, experiment, and compare with open source solvers as **GPOPS**
- ❑ **Space debris mitigation** with space robots
- ❑ Interdisciplinary possibilities:
 - Collaboration with **Nonlinear Dynamical Control Systems and Spacecraft Engineering Research Lab** on under-actuation and failures
 - Collaboration with **Atmospheric Physics Research Lab.** and **Computational Atmospheric Dynamics Lab** for differential drag developments
 - Start/Expand nano-satellites **and CubeSats programs**
 - **Develop Embry-Riddle program on small satellites for real flight!**
- ❑ **GOOD MANAGEMENT IS A MUST**

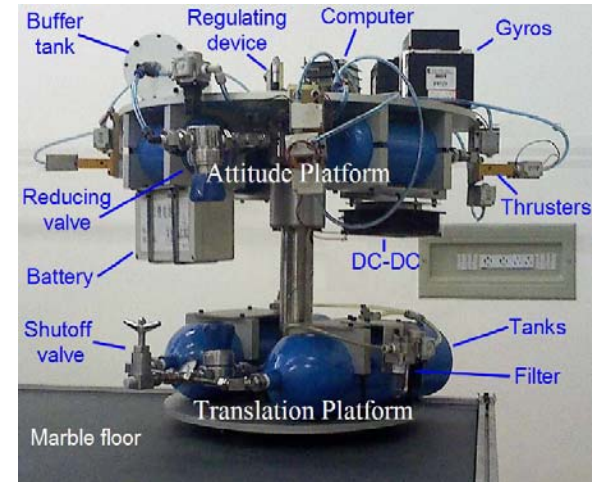
External Collaborations

- Keep the ongoing collaboration with School of Aerospace Engineering, University “Sapienza” of Rome, Italy.
- Continue interaction with Canadian Space Agency
- Establish a collaboration between Embry-Riddle and the Naval Postgraduate School.
- Establish a collaboration between Embry-Riddle and MIT (I have been partially involved with the SPHERES project)
- Establish a collaboration between Embry-Riddle and WVU (new satellites refueling center coming soon)
- Establish a collaboration between Embry-Riddle and the University of Florida on Optimization of Multiple Spacecraft Maneuvers.
- Establish a collaboration between Embry-Riddle and the CalPoly/Mathworks for software support for CubeSats

6 DOF Spacecraft Simulator



Granite / Epoxy / "Hockey" table / Synthetic Ice



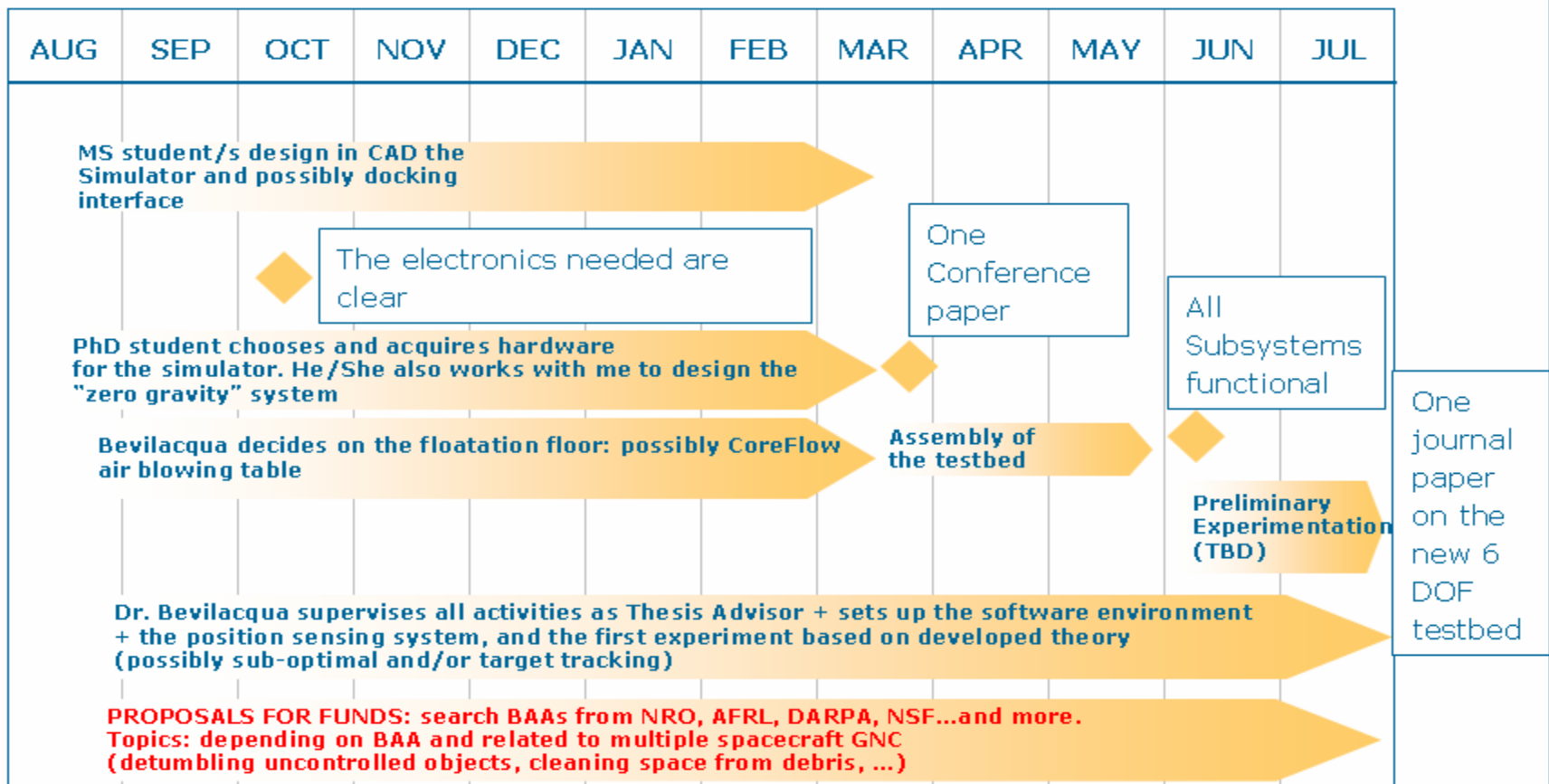
5DOF simulator Research Center of Pneumatics Harbin Institute of Technology. Harbin, China



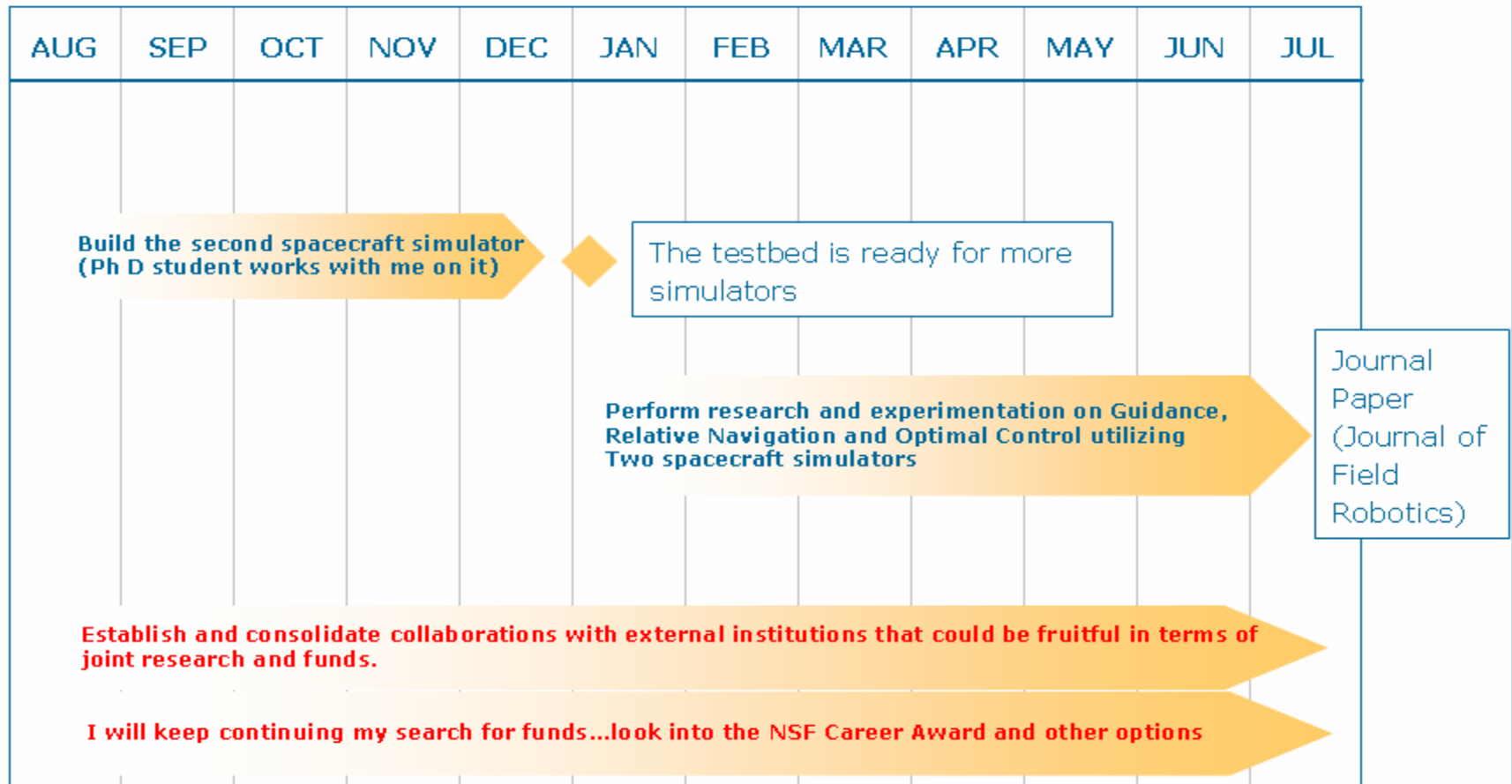
Constant force springs

CHECK TRANSFER FUNCTION

Year I (building 1st simulator & search for ext. funds)



Year II (we have funds!)



Proposals for Funds

- DARPA (www.FedBizOpps.gov , explore and register to receive real-time notifications)
- NRO (Director's Innovation Initiative: <https://dii.westfields.net/>)
- AFRL (www.FedBizOpps.gov)
- NASA (NSPIRES website for solicited proposal, http://prod.nais.nasa.gov/pub/pub_library/unSol-Prop.html, for unsolicited)
- NSF (<http://www.nsf.gov/funding/azindex.jsp?start=S>, example: CubeSat weather program)
- www.grants.gov
- <http://www.library.uiuc.edu/iris/>
- ...this comes from my experience at NPS...and I know Embry-Riddle can rely on private funding, NSF, and more.

□ Existing courses

BS

- ES 204 Dynamics
- MA 245 Differential Equations and Matrix Methods
- PS 215 Physics I
- PS 208 Physics II
- PS 219 Physics III
- EP 340 Introduction to Space Systems Design
- EP 393 Spaceflight Dynamics
- EP 394 Space Systems Engineering

MS

- EP 505 Advanced Spacecraft Dynamics and Control
- EP 600 Experimental Methods in Space Science
- MSE 545 Specification and Design of Real-Time Systems
- MSE 655 Performance Analysis of Real-Time Systems

□ Proposed courses

- Spacecraft Attitude Dynamics
- Advanced Attitude Determination and Control
- DESIGN OF SPACECRAFT GNC FOR REAL-TIME TESTING

The new Ph.D. program at Embry-Riddle

My areas of interest

- Spacecraft Instrumentation
- Spacecraft Systems Engineering
- Dynamics and Control of Aerospace Systems
- Space Robotics/Autonomous Systems

Courses

- | | |
|---------------------------------|---|
| <input type="checkbox"/> EP 702 | Theoretical Mechanics and Astrodynamics |
| <input type="checkbox"/> EP 705 | Optimal Dynamical Systems |
| <input type="checkbox"/> EP 707 | Nonlinear Dynamical Control Systems |
| <input type="checkbox"/> EP 709 | Stochastic Systems in Engineering Physics |

